Agra Smart City Mission

Improvements to Taj East Drain

DPR

Submitted by:







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EXECUTIVE SUMMARY

• Introduction

The smart city project for Agra is earmarked for about 22.50 Hectares covering both side of Fatebad road and Taj Ganj area around Taj Mahal. Taj East drain is one of major drain flows across the ABD area. It originates from Shamshabad road as a road side drain along Gobar Chowki road and crosses Fatebad road further merges as single drain near Nageena Masjid and further collecting the inflow from the catchment area crossed Taj east road and confluence at river Yamuna. The total length of drain is about 4000 mts.

• Existing condition of Taj East Drain

The storm water drain is slowly turned into sewage and solid waste disposal due to lack of adequate sewerage and solid waste infrastructure. The drain is also travels through thickly populated urban area. Part of the drain also passes through ABD area from ch.1520 to ch.4000

At present the drain during dry weather flow carries domestic sewage and solid waste. Though the catchment area is having sewerage facilities 100% house sewer connections are not yet commissioned. Due to this the public health of people living at vicinity of the drain are affected. As this drain crosses near to Taj Mahal it also affects aesthetics of Taj Mahal.

As these drain confluence to river Yamuna, the pollution level is so high that the river Yamuna lost its self-cleaning capacity and carries only sewage and effluents discharged from various industries. As a immediate measure to curb pollution to river Yamuna Jal Nigham has installed a sewage pumping station at Kolhai and the drain flow is diverted to SPS and further pumped to STP at Dandhupura for further treatment and disposal.

• Proposed improvements to Taj east drain

The total catchment area of the drain is about 2369 hectares covering within municipal limit and outside the limit. The total area is divided into 7 catchment zones. The drain is designed as per CPHEEO guidelines for its carrying capacity and improvement plan is proposed to improve the existing drain and constructing new drain from Taj east road junction at chainage 3215m to confluence point at river Yamuna chainage 4000m.

From chainage from 0m to 680m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain.



- 1. Rising of side wall
- 2. Plastering of exposed brickwork inside of drain
- 3. Providing RCC cover slab
- 4. Providing grating arrangements with rainwater harvesting structures

From chainage from 680m to 810m the existing drain size is closed with RCC slab and serving as road. So, no improvement works are proposed except desigling and disposing of silt and solid waste.

From chainage from 810m to 1800 (R), 1520 (L) the existing drain size is inadequate for hydraulic adequacy. The following works are proposed for strengthening of drain

1. Construction of new RCC drain with cover slab and grating arrangement

From chainage from 2040m to 3120m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain

- 1. Rising of protection wall on both side of the drain with brickwork
- 2. Plastering of inside exposed brickwork
- 3. Providing cover slab with ventilation shaft for air ventilation
- 4. Providing grating arrangements with rain water harvesting structures

From chainage from 3120m to 3215m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain

- 1. Construction of new side wall
- 2. Plastering of inside exposed brickwork
- 3. Providing cover slab with ventilation shaft for air ventilation
- 4. Providing grating arrangements with rain water harvesting structures

From chainage from 3215m to 4000m new adequate drain size is proposed for hydraulic adequacy. The following works are proposed for construction of new drain

1. Construction of new RCC drain as per the hydraulic and structural design requirements with rain water harvesting structures

Apart from above improvements screen chambers with screen arrangements are proposed at junctions where lateral drains join Taj East drain

• Cost estimate

Detailed cost estimate has been prepared using Agra PWD schedule of rates and data has been worked out for non-schedule of rates as per market rates

Total project cost worked out to be **17.20** Crores.

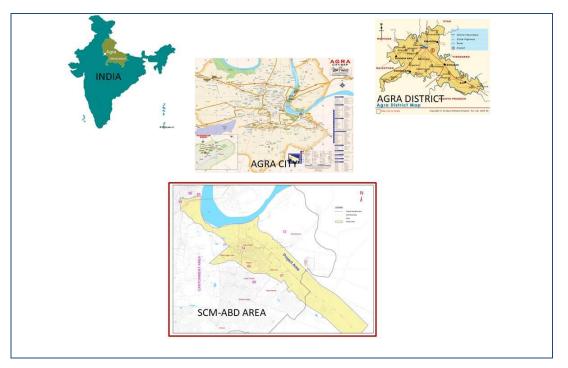


1.0. Preamble

Uttar Pradesh is urbanizing much more slowly than other parts of India. At 11.8%, its urban population is one third of the average urban population of India (31.6%, Census, 2011). Even though urban population may be growing slowly, Agra is one of the important city in Uttar Pradesh

Agra city is located on the southern bank of river Yamuna. It is a northern part of Uttar Pradesh, India. The state capital Lucknow is about 378 Km on east. Agra is near national capital New Delhi about 206 Kms northwest direction. The city is also well connected with National highways, rail networks to other major cities and district headquarters.

Agra is a major tourist destination because of its many Mughal-era buildings, most notably the Tāj Mahal, Agra Fort and Fatehpur Sikri, all three of which are UNESCO World Heritage Sites. Agra is included on the Golden Triangle tourist circuit, along with Delhi and Jaipur; and the Uttar Pradesh Heritage Arc, tourist circuit of UP state.





The climate of Agra experiences mild winters, hot and dry summers and a monsoon season. Agra has a reputation of being one of the hottest towns in India. In summers the city witnesses a sudden surge in temperature and at times, mercury goes beyond the 46°C mark in addition to a very high level of humidity. During summer, the daytime temperature hovers around 46-50°C. Nights are relatively cooler and temperature lowers to a comfortable 30°C. Winters are bit chilly but are the best time to visit Agra. The minimum temperature sometimes goes as low as 2 or 3°C but usually hovers in the range of 6 to 8°C.





Agra is one of 13 cities selected for smart city mission by Govt. of India, ABD area is earmarked based on selection criteria as follows

- The city profile
- Citizen opinion and engagement
- Opinion of the elected representatives
- Discussion with the urban planners and sector experts
 - Discussion with the suppliers/ partners

The ABD area covers about 2.40 % of total Municipal corporation area. Two villages Kalal Kheria and Mayapura is located adjacent to the Municipal limit is also added to ABD area.

Taj east drain is one of the primary storm water drain flowing within ABD area flows from south to north direction. It originates as road side drain at chainage 0 to confluence point at Yamuna

2.0. **Demographics**

Agra is a major tourist destination because of its historical Mughal-era buildings, three historical monuments are earmarked for UNESCO World Heritage sites.

- 1. Taj Mahal,
- 2. Agra Fort
- 3. Fatehpūr Sikrī,

Agra City with a total land area of 141 km² had a population of 2,22,943 in 2011. The growth rate of Agra varies from decade to decade and last three decade the growth rate is increasing. In last six decades the population has grown almost 4.75 folds, with increase in population from 3,33,530 in 1951 to 15,85,704 in year 2011. The growth pattern of the town is illustrated in the Table 1.

| SI. | | Рори | lation | Decadal Growth |
|-----|------|------------|-----------|--------------------------------|
| No. | Year | Population | Variation | rate Population Variation % |
| 1 | 1951 | 333530 | | |
| 2 | 1961 | 462020 | 128,490 | 39% |
| 3 | 1971 | 591917 | 129,897 | 28% |
| 4 | 1981 | 694191 | 102,274 | 17% |
| 5 | 1991 | 891790 | 197,599 | 28% |
| 6 | 2001 | 1275134 | 383,344 | 43% |
| 7 | 2011 | 1585704 | 310,570 | 24% |
| 8 | 2035 | 2396855 | 811,151 | 51% |

Table 1: Decadal Population and Growth Pattern



Agra recorded an overall literacy rate of 60.10 % with female literacy of 40.96%, Thus Agra compares favourably in terms of literacy and sex ratio compared to state averages on these indicators.

3.0. Existing condition of Taj east drain

The drain originates from Shamshabad road junction at ch-0m and confluence to river Yamuna at Ch-4000m. Taj East drain carries storm water during monsoon season and domestic sewage during arid season. Almost 85% of all household toilets in the low- income settlements along the drain directly or through shallow surface drains discharge faecal matter directly into the drain. Trade waste both liquid and solid also flows through the drain. Besides creating highly unsanitary conditions, the drain floods every monsoon causing loss of life and property. Over the years, it has also silted reducing its carrying capacity and increasing the incidence of flooding.

There are 17 low- income settlements along the drain's edge. The area also has some of the most luxurious hotels in the city such as the Amar Vilas and Mughal Sheraton besides traditional Mughal residential areas or Katras. There are some middle- income residential areas also in the Tajganj area. Taj East drain is discharged with both solid and liquid waste water that is generated from these habitations. It is estimated that waste water in the drain must be generated from approximately in wards 70, 71, 74, 80 and parts of 72 and 89.

Sewer lines are being laid in the area but are expected to cover only about 60% of households in the area along the drain. These are however, yet to be made operational. There is a gap in providing house sewer connections in areas where sewer lines are laid. are provided and also many households didn't have toilet facilities.

The alignment of drain flows through the following global coordinates.

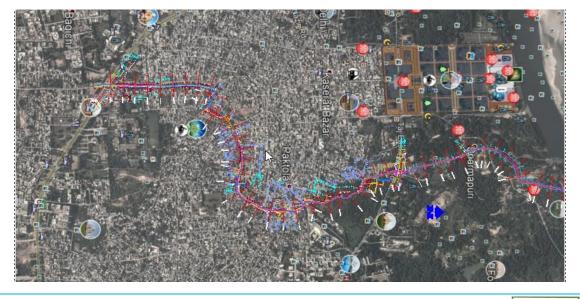
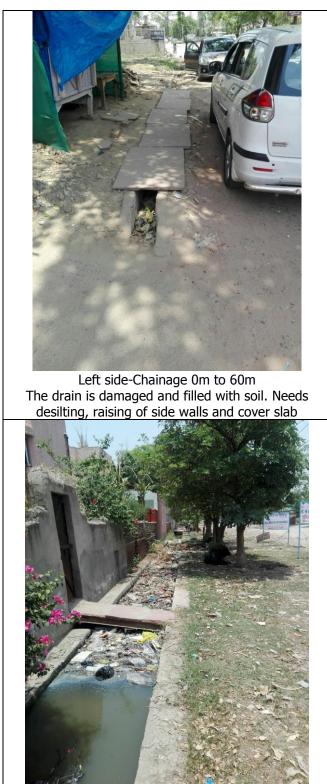


Figure 2: Taj East Drain

STC







Left side-Chainage 60m to 300m The drain is open, silted and filled with solid waste. Needs desilting, raising of side walls and cover slab



Right side-Chainage 0m to 60m The drain is open and filled with solid waste Needs desilting, raising of side walls and cover slab



Right side-Chainage 90m to 300m The drain is open, silted. Needs desilting, raising of side walls and cover slab







Left side-Chainage 520m to 670m The drain cross from left to right

Right side-Chainage 520m to 600m The drain is open, heavily silted & exposed brickwork







STC





Left side-Chainage1520m to 2040m Open drain with exposed brick work heavily silted and partially covered by residents



Right side-Chainage 1520m to 2040m The drain is open, heavily silted & exposed brickwork



Chainage 2040m to 2130m vulnerable for flooding The drain is open ,filled with solid waste, silted exposed brickwork without cover slab



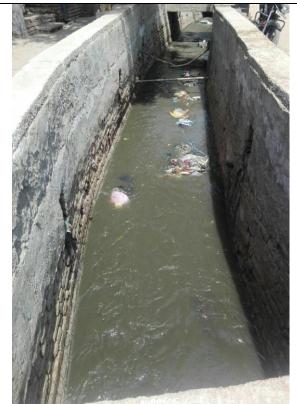
Chainage 2160m to 2190m road crossing The drain is open, heavily silted, no protection wall on sides and no cover slab







Chainage 2190m to 2340m The drain is open, heavily silted, protection wall needs to be raised and uncovered



Chainage 2340m to 2430m The drain is open, silted, protection wall needs to be raised and uncovered



Chainage 2420m to 2450m Road culvert crossing Solid waste dumping yard drain is open, heavily silted, protection wall needs to be raised and uncovered



Chainage 2450m to 2820m Open exposed brickwork drain, Desilting, Protection walls need to be raised, cover slab to be provided







STC





Chainage 3210 crossing near Taj east gate road Open drain without side walls, heavily silted by sliding of soil and needs to be refurbished with brickwork and plasterin



Chainage 3230 to 3480 after crossing near Taj east gate road Open drain partially damaged, silted without side protection wall, needs desilting, construction of damaged walls, plastering and cover slab



Table 2: Condition assessment and improvement matrix for Taj east drain

| | | | C | Condition assessment a | and improvement plan fo | r Taj east drain | from Shamsh | abad roa | d to confluence po | oint at Riv | ver Yamuna | | |
|------------------|--------------------------------------|---------------------------|----------------------|--|---|--|-----------------|--|--------------------------|----------------------|---|--|--|
| Left side | | | | | | | | Right side | | | | | |
| Chainag e (m) | Size of drain B (m) x D (m) | Constructio n material | Silt depth (m) | Condition assessment | Improvements | Remarks | Chainage (m) | Size of drain B (m) x D (m) | Construction material | Silt depth (m) | Condition assessment | Improvements | Remarks |
| 0-60 | | | | No drain is visible | Minimum size drain shall be provided | | 0-60 | 0.90 x 1.30 | Exposed brick work | 0.9 | Side walls are lower than GL, Heavily silted, No cover slab | Desilting of drain, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | At 60m rightside drain joins leftside drain by culvert crossing |
| 60-520 | 1.50 x 1.50 | Exposed brick work | 1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | At 520 the drain crosses to right and joins rightside drain | 90-380 | 1.20 x 1.30 | Concrete wall | 1 | Side walls are lower than GL, Heavily silted, No cover slab | Desilting of drain, rising of side walls for 0.45m above ground level, & providing cover slab | At 520 leftside drain joins right side drain |
| | | | | | | | 380-520 | 1.2 x 1.8 | Exposed brick work | 1.3 | Side walls are lower than GL, Heavily silted, No cover slab | Desilting of drain, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | |
| | | | | | | | 520-680 | 1.2 x 1.8 | Exposed brick work | 1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | |
| | | | | | | | 680-810 | | Closed drain | | The drain is closed with RCC slab with manholes. Drain is serving as road | Desilting and disposal of silt & debris is required | The exact condition is not visible |
| 810-930 | 1.0 x 1.50 | Exposed brick work | 1.1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | at 810 confluence to side drain | | | | | | | |
| 930-1140 | 1.2 x 1.3 | Exposed brick work | 0.9 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & | | | | | | | | |

STC



| | Condition assessment and improvement plan for Taj east drain from Shamshabad road to confluence point at River Yamuna | | | | | | | | | | | | |
|------------------|---|---|----------------------|---|---|---------|-----------------|--|---|----------------------|---|--|--|
| | Left side | | | | | | | | Ri | ght side | | | |
| Chainag e (m) | Size of drain B (m) x D (m) | Constructio n material | Silt depth (m) | Condition assessment | Improvements | Remarks | Chainage (m) | Size of drain B (m) x D (m) | Construction material | Silt depth (m) | Condition assessment | Improvements | Remarks |
| | | | | | providing cover slab | | | | | | | | |
| 1140- 1500 | 1.2 x 1.3 | Exposed brick work | 1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | | 1450-1500 | .90 x .50 | Exposed brick work | 0.3 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | |
| 1550- 1800 | 1.4 x 1.3 | Stone boulders (RR masonery), Partially covered by shops | 1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | | 1500-2040 | .90 x .80 | Stone boulders (RR masonery), Partially covered by shops | 1 | Heavily silted with solid waste, side walls are lower than GL & no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab | At 2040 drain cross to left side and joins as major drain. The area is prone to flooding |
| 1800- 2040 | .45 x .60 | Exposed brick work | 0.5 | Heavily silted, side walls are lower than GL & no cover slab. The drain size is reduced | Desilting and disposal of silt & debris, rising of side walls for 0.45m above ground level, inside plastering & providing cover slab. Adequacy for carrying capacity to be checked | | | | | | | | |



| Chainage (m) | Size of drain B (m) x D (m) | Construction material | Silt depth (m) | Condition assessment | Improvements | Remarks |
|-----------------|-----------------------------------|--|----------------------|--|---|--|
| 2040-2130 | 1.0 x 1.20 | Brickwork drain with plastering | 1 | Heavily silted with solid waste, side walls are at GL and no cover slab | Desilting and disposal of silt & debris, rising of side walls for 0.60m above ground level & providing cover slab | |
| 2160-2190 | 2.0 x .80 | Closed drain in brickwork with plastering | 0.5 | Closed by road crossing culvert. Side walls of culvert are unplastered | Road culvert crossing | At 2190 mechanical screen may be provided to remove solid waste |
| 2190-2270 | 2.0 x 1.0 | Exposed brick work with side walls raised upto .45m | 0.5 | Silted with grit sludge. Side walls unplastered | Desilting and disposal of sludge and grit, rising of side walls uniformly to 0.60m above ground level & providing cover slab | |
| 2270-2300 | 2.0 x 1.0 | Closed drain | 0.5 | Silted with grit sludge. Side walls unplastered | Desilting and minor repair works needed | |
| 2300-2430 | 2.0 x 1.0 | Exposed brick work with side walls raised upto .60m | 0.4 | Silted with grit sludge. Side walls unplastered | Desilting, Side wall plastering required | At 2430 mechanical screen may be provided to remove solid waste |
| 2430-2670 | 2.90 x 2.0 | Exposed brick work with side walls raised upto .40m | 0.6 | Silted with grit sludge. Side walls unplastered | Desilting and disposal of sludge and grit, rising of side walls uniformly to 0.60m above ground level & providing cover slab | At 2670 major drain joins from right side 2.0 x 2.5 |
| 2670-2850 | 3 x 2.5 | Exposed brick work with side walls raised upto .40m | 0.75 | Heavily silted with solid waste, left side side wall is good, right side sidewall needs to be raised for 2m to avoid soil sliding into drain | Right side sidewall to be raised, plastering of side walls with cover slab to be provided | |





| 2850-2960 | 5 x 3 | Exposed brick work | 1 | The side walls are collapsed during recent flood, | Both side walls to be constructed with cover slab |
|-----------|-------|-----------------------|-----|--|--|
| 2960-3060 | 5 x 3 | Exposed brick work | 0.8 | The side walls partially damaged | Both side walls to be constructed with cover slab |
| 3060-3090 | 4 x 5 | Exposed brick work | 0.7 | Both side walls are damaged | Both side walls to be constructed with cover slab |
| 3090-3210 | 6 x 5 | Exposed brick work | 0.7 | Both side walls are partially damaged | Rehabilitation of walls and cover slab is needed |
| 3210-3480 | | Exposed brick work | | Side walls are partially damaged | Rehabilitation of side walls, rising above GL for o.60m and cover slab is needed |
| 3480-4000 | | Earthern drain | | Wide earthern drain of 26m wide | New drain to be constructed |

Condition assessment survey for the entire stretch from chainage 0 to 4000 has been carried out and improvement plan has been worked out

4.0. Need of the project

The storm water drain is slowly turned into sewage and solid waste disposal due to lack of adequate sewerage and solid waste infrastructure. The drain is also travels through thickly populated urban area. Part of the drain also passes through ABD area from ch.1520 to ch.4000. At present the drain during dry weather flow carries domestic sewage and solid waste. Though the catchment area is having sewerage facilities 100% house sewer connections are not yet commissioned. Due to this the public health of people living at vicinity of the drain are affected. As this drain crosses near to Taj Mahal it also affects aesthetics of Taj Mahal. So there is an urgent need for this project and bring the drain to its original condition.

During the heavy rains and floods, the infrastructure (roads, drains etc,) are being damaged and needs repairs and re-strengthening works. A huge amount is being spent on this account. In addition the floods are also having impact on human health (spreading of water borne diseases and Vector Borne diseases).

As these drain confluence to river Yamuna, the pollution level is so high that the river Yamuna lost its self-cleaning capacity and carries only sewage and effluents discharged from various industries. As a immediate measure to curb pollution to river Yamuna and bring back the drain to its original condition this project is vial.



5.0. Sewage pumping station at Kolhai

As a immediate preventive measure to curb discharge of sewage into Yamuna river UP Jal Nigham installed a Sewage Pumping Station (SPS) adjoining to drain at chainage 2700 Km at Kolhai Shutter provision with screen arrangements are provided across the drain to divert the flow sewage pumping station and further it is pumped to Sewerage Treatment Plant (STP) at Dhanadupura. At present about 18 MLD of sewage is pumped from this pumping station to STP. However sewage from downstream of this pumping station sewage infalls into the drain from 2 large settlement settlements, 2 katras at the south gate of Taj Mahal, and a few middle income residential area is flowing untreated into Yamuna river.

6.0. **Objectives of the assignment**

The project shall have two key objectives:

- 1. To check the hydraulics of the drain to discharge storm water effectively without inundations into river Yamuna.
- 2. To bring back the drain to its original form by curbing discharge of domestic sewage and solid wastes into the drain thereby the pollution caused by this drain to Yamuna can be stop sewage and solid waste pollution discharged into Yamuna by improving the sewage infrastructure for Agra especially to the catchment areas of the drain.
- 3. To study and improve the Taj east drain infrastructure to achieve effective storm water drainage system of Taj ganj area.

7.0. Survey and investigations

7.1. Reconnaissance Survey

The reconnaissance survey shall cover the entire Taj east drain system and shall form the basis for identification of the extent of the field surveys, studies / investigation. As a minimum, the following features shall be identified.

- Location of obstructions types, cause etc.
- Location of encroachments
- Location of low-lying areas extent, general ground level, type of establishment etc.
- Locations of culverts / bridges / pedestrian crossings etc.
- Location of existing wastewater / sewage disposal points to open drain

7.2. **Topographical Survey & Investigations**

The following survey & investigations have been carried out which are required for the design activity and will be carried out through our experienced surveyors with sophisticated survey equipment.





7.3. Site Survey:

 Site Plans (drawn to suitable scales) showing sufficient details including location, levels, high flood levels and ground water table, approaches, existing buildings, encroachments etc. for following components:

7.4. Alignment survey:

Alignment survey along the entire proposed alignment for drainage collection system, natural drains (nallas), with levels cross sectional details survey of natural nalla's will be conducted. Bearings along the alignment to be recorded and L-sections showing following features are plotted:

- Plan of the alignment
- Cross drainage works (bed level, size of culvert, width of cross drainage)
- Drain crossings with levels along bed, river width, high flood level, details of adjacent existing bridges
- Road and railways Crossings
- Details of roads adjacent to the alignment
- Details of encroachments, structures, power & telephone lines etc. along and across the alignment
- High flood levels and ground water tables recorded at every 500m along the course of the natural drains.

8.0. Approach & Methodology

- Based on the water sheds, the carrying capacities of the existing drains are being assessed and analysed for hydraulic adequacy with help of Bentley StormCAD V8i software's.
- Following improvement of existing hydraulic adequate road side drain will be proposed
 - Desilting and safe disposal of silt and solid waste from the drain
 - Raising of side wall to avoid in fall of soil from road into drains
 - Plastering of drain side wall with SRC cement to prevent corrosion from sulphate attack
 - Providing cover slab to protect the drain from solid waste fill
 - Providing grating arrangements at regular interval to allow rain water to flow into drain
- Following improvement of existing hydraulic adequate major open drain will be proposed





- The protection wall on both side of the drain shall be raised to safeguard the residents adjoining to drain
- Plastering of drain inside with SRC cement mortar to protect the structure from sulphate attack
- Providing cover slab to protect the drain from solid waste fill
- Providing grating arrangements at regular interval to allow rain water to flow into drain
- Wherever the side walls are damaged, new side walls with brickwork shall be proposed
- Wherever side walls are partially damaged retrofitting the walls with new brickwork shall be proposed
- Wherever earthen drains are identified, new drain with RCC walls shall be proposed

8.1. Design criteria for Strom Water Drains

General specification for Construction Material Proposed for new drain / Channel/Culvert as recommended by IS 456-2000 and other codes

Cement : The cement shall be Ordinary Portland Cement of 43 grade conforming to IS:8112. It is proposed to use sulphate resisting cement (SRC) to prevent corrosion of structure due to sulphate attack. Other specifications for storage, testing etc. shall be as per the relevant IS codes.

Aggregate: All the aggregate (coarse and fine) shall conform to the technical specification laid down under relevant IS code 383-1987. Unless otherwise specified, well graded coarse aggregate of 20mm size shall be used in reinforced cement concrete for drain wall, base slab and cover slab. For plain cement concrete too, graded 20mm size aggregate shall be used.

Water: Clean water for mixing and curing shall be free from injurious amounts of oils, acids, alkalis, salts, sugar, organic materials or other substances that may be deleterious to the concrete and steel and should confirm to the specifications laid IS:456 - 2000.

Admixtures: If required, chemical admixture in concrete shall be used as specified in IS:456-1978.

Reinforcement: Epoxi coated Mild steel and high tensile steel bars and hard drawn steel conforming to IS:432 (Pt-I)-1982. Cold twisted worked bars conforming to IS:1786- 1985 and hard drawn steel wire and fabric conforming to IS:1566-1982 shall be used and structural steel section conforming to IS:226-1975 shall be used.



8.2. Structural design of Drains

The engineer shall specify the material type to be used in the conduit for the underground drainage system. The material type shall be Reinforced concrete Drain of M-25 Grade, Density of concrete used 25KN/ m³, Fe 415 Grade Steel used.

The drains are designed for two conditions

- 1. Drain full of water and no earth pressure from outside
- 2. Earth pressure from outside and no water in the drain

Drains Section to be provided Bottom sand filling 100mm, Levelling course using M 10 concrete 100mm thick and Bottom slab with RCC M25 concrete.

Drains have been provided with cover slab, Pre cast RCC Slabs are provided at regular intervals of 15 m to facilitate for cleaning purpose.

Gratings have also been provided at every 15m interval. The cover slab has been designed for live load and dead load.

Culvert

The Culverts are proposed at every road junctions and for crossing from one side to other side of the roads . The minimum size of the culverts is 2.0m x 2.0m Box culverts are suggested for adoption. It has been designed as RCC box culvert of M 25 concrete with live load (superimposed load) considered IRC Class AA loading, Density of concrete used 25KN/m³, Fe 415 Grade Steel used.

Box culvert wall has been designed for the following four conditions

- 1. Culvert full of water and no earth pressure from outside
- 2. Earth pressure from outside and no water in the culver
- 3. Dead load and live load with no water in the culvert

Code References: IS:426-2000, IS 3370 Part III, IRC SP 6 and SP 13

9.0. Rainfall Analysis / Interpretation

The most important factor determining the size of storm water drain is the intensity of rainfall, which varies inversely to the duration. For any drain section, the intensity of rainfall corresponding to a duration equal to the time of concentration (time taken for storm water from the extreme end of the catchments to reach the point under consideration) at that section only will give the maximum flow.





- Time of Concentration also decides the economical section of the drain.
- The inadequate design factors and inadequate size of the drains will lead to either inundation or further damage to the existing storm water drainage system as well as the structures on the banks.
- Rainfall intensities and its return period are the critical factors in the design of any storm water drainage system.
- The size of the drain for a particular section needs to be designed to carry the runoff contributed by the respective catchment area.
- The topography of the contributing area also plays a major role.

The rainfall data available for Agra for 24 hour rainfall depth for a period of 30 years (1981 to 2012) were collected from the Indian Meteorological Department (IMD), Pune. The yearly maximum precipitation for past 30 years is furnished below:

| S.No | Year | Maximum Annual One Day Rainfall (mm) | Total Annual Rainfall (mm) |
|------|------|--|-------------------------------------|
| 1 | 1981 | 365 | 511.5 |
| 2 | 1982 | 191.5 | 1086.2 |
| 3 | 1985 | 285 | 1011.2 |
| 4 | 1986 | 60 | 118.8 |
| 5 | 1987 | 500 | 500.5 |
| 6 | 1988 | 69.2 | 440.6 |
| 7 | 1989 | 85.6 | 285.1 |
| 8 | 1990 | 15 | 38.6 |
| 9 | 1991 | 8.1 | 34.2 |
| 10 | 1992 | 51 | 289.2 |
| 11 | 1993 | 204 | 452 |
| 12 | 1994 | 55 | 160.7 |
| 13 | 1995 | 49 | 329.7 |
| 14 | 1996 | 180 | 407 |
| 15 | 1997 | 34 | 78.8 |

Table 4 : Rainfall data for 30 years period

| S.No | Year | Maximum Annual One Day Rainfall (mm) | Total Annual Rainfall (mm) |
|------|---------|--|-------------------------------------|
| 16 | 1998 | 54 | 101.6 |
| 17 | 1999 | 60 | 169 |
| 18 | 2000 | 27 | 123.7 |
| 19 | 2001 | 16.1 | 79.3 |
| 20 | 2002 | 66.2 | 200.3 |
| 21 | 2003 | 55 | 184.9 |
| 22 | 2004 | 32 | 179.8 |
| 23 | 2005 | 68 | 228 |
| 24 | 2006 | 44 | 187.4 |
| 25 | 2007 | 52 | 75 |
| 26 | 2008 | 70 | 194 |
| 27 | 2009 | 12.6 | 22.5 |
| 28 | 2010 | 64 | 186 |
| 29 | 2011 | 58 | 170.4 |
| 30 | 2012 | 160 | 560 |
| | Average | 99.71 | 280 |



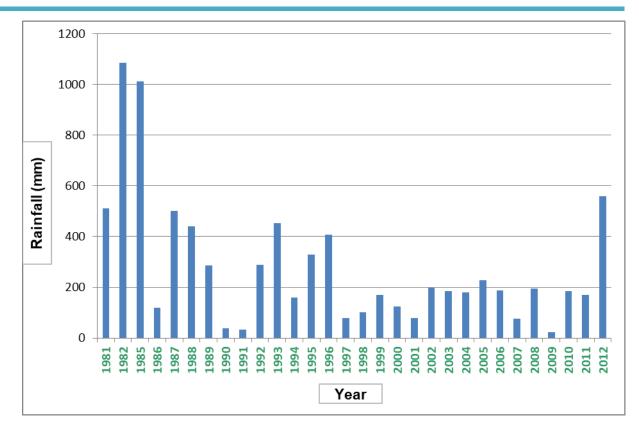


Figure 4: Graph showing the Maximum Total Annual rainfall for 30 years period

Rain fall has exceeded the average rain fall for about 9 years and for major periods the annual rain fall is below average.

To generate IDF curves and for forecasting the rain fall intensities for various return periods, the following statistical methods are adopted.

- Method based on Least Squares Principle
- Annual exceedance with IMD 1/3rd Rule Method & Gumbel's equation

9.1. Method based on Least Squares Principle

This is a statistical method used to determine a line of best fit by minimizing the sum of squares created by a mathematical function. A "square" is determined by squaring the distance between a data point and the regression line.

The least square equation for linear regression is $\mathbf{Y} = \mathbf{A} + \mathbf{B}\mathbf{X}$ Where,

Y = Dependent variable computed by the equation

A = y intercept, B = Slope of the line, X = Time period



The least square method tries to fit the line to the data that minimize the sum of the sum of the squares of the vertical distance between each data point and its corresponding point on the line.

In the least square method, the equations for A' and B' are

$$A = \bar{y} - B\bar{x}$$

and

$$B = \frac{\sum \bar{x}\bar{y} - n \bar{x}\bar{y}}{\sum x^2 - n x^2}$$

As far as the rainfall data are concerned,

Y = Max annual one day rainfall mm/day

$$X = \log\left(\log\frac{T}{T-1}\right)$$

Recurrence Interval in years T = (N+1)/m

N = number of years = 27

m = ranking number

Table 5 : Rainfall analysis by Least Square Method

| Ranking "m" | Year | Max annual one day rainfall mm/day "y" | Total annual rainfall (mm) | Recurrence Interval in years T=(N+1)/m | x = loglogT/T-1 | ху | x ² |
|----------------|------|---|-------------------------------------|---|--------------------|----------|-----------------------|
| 1 | 1987 | 500 | 500.5 | 30.0 | -1.832 | -915.998 | 3.356 |
| 2 | 1981 | 365 | 511.5 | 15.0 | -1.523 | -556.045 | 2.321 |
| 3 | 1985 | 285 | 1011.2 | 10.0 | -1.340 | -381.768 | 1.794 |
| 4 | 1993 | 204 | 452 | 7.5 | -1.207 | -246.141 | 1.456 |
| 5 | 1982 | 191.5 | 1086.2 | 6.0 | -1.101 | -210.914 | 1.213 |
| 6 | 1996 | 180 | 407 | 5.0 | -1.014 | -182.454 | 1.027 |
| 7 | 1989 | 85.6 | 285.1 | 4.3 | -0.938 | -80.277 | 0.880 |
| 8 | 2008 | 70 | 194 | 3.8 | -0.871 | -60.945 | 0.758 |
| 9 | 1988 | 69.2 | 440.6 | 3.3 | -0.810 | -56.048 | 0.656 |
| 10 | 2005 | 68 | 228 | 3.0 | -0.754 | -51.290 | 0.569 |
| 11 | 2002 | 66.2 | 200.3 | 2.7 | -0.703 | -46.507 | 0.494 |
| 12 | 2010 | 64 | 186 | 2.5 | -0.654 | -41.852 | 0.428 |
| 13 | 1986 | 60 | 118.8 | 2.3 | -0.608 | -36.473 | 0.370 |
| 14 | 1999 | 60 | 169 | 2.1 | -0.564 | -33.830 | 0.318 |
| 15 | 2011 | 58 | 170.4 | 2.0 | -0.521 | -30.241 | 0.272 |
| 16 | 1994 | 55 | 160.7 | 1.9 | -0.480 | -26.410 | 0.231 |
| 17 | 2003 | 55 | 184.9 | 1.8 | -0.440 | -24.193 | 0.193 |
| 18 | 1998 | 54 | 101.6 | 1.7 | -0.400 | -21.610 | 0.160 |
| 19 | 2007 | 52 | 75 | 1.6 | -0.361 | -18.761 | 0.130 |
| 20 | 1992 | 51 | 289.2 | 1.5 | -0.321 | -16.390 | 0.103 |
| 21 | 1995 | 49 | 329.7 | 1.4 | -0.282 | -13.798 | 0.079 |
| 22 | 2006 | 44 | 187.4 | 1.4 | -0.241 | -10.607 | 0.058 |
| 23 | 1997 | 34 | 78.8 | 1.3 | -0.199 | -6.775 | 0.040 |
| 24 | 2004 | 32 | 179.8 | 1.3 | -0.156 | -4.977 | 0.024 |

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-25.520



| Ranking "m" | Year | Max annual one day rainfall mm/day "y" | Total annual rainfall (mm) | Recurrence Interval in years T=(N+1)/m | x = loglogT/T-1 | ху | x ² |
|----------------|------|---|-------------------------------------|---|--------------------|---------------|-----------------------|
| 25 | 2000 | 27 | 123.7 | 1.2 | -0.109 | -2.941 | 0.012 |
| 26 | 2001 | 16.1 | 79.3 | 1.2 | -0.058 | -0.933 | 0.003 |
| 27 | 1990 | 15 | 38.6 | 1.1 | 0.000 | 0.000 | 0.000 |
| 28 | 2009 | 12.6 | 22.5 | 1.1 | 0.070 | 0.888 | 0.005 |
| 29 | 1991 | 8.1 | 34.2 | 1.0 | 0.169 | 1.372 | 0.029 |
| | | | | | | | |
| N = 29 | Sum | | | | | - 3075.919 | 16.978 |
| | Mean | 97.6 | 270.6 | | -0.595 | | |

 $= 97.6 \\ -0.595 \\ 0.3536 \\ B = -207.088$

So
$$B = \frac{\sum \overline{x} \overline{y} - N \overline{x} \overline{y}}{\sum x^2 - N \overline{x}^2}$$
$$A = \overline{y} - B \overline{x}$$

Mean y

Mean x

$$F = A + B \log \left(\log \frac{T}{T-1}\right)$$
$$I_0 = \frac{F}{T} \left[\frac{T+1}{t_c+1}\right]$$

F - Maximum rainfall in T hours (Here, 24 hours)

А

=

T = 24 hours

 $t_{\mbox{\scriptsize c}}$ - Time of concentration in hours

| T = 1.1 | -29.16746034 | | -Io = 15.19 | |
|---------|--------------|----|-------------|-------|
| T = 1.5 | F = 41.03 | mm | Io = 21.37 | mm/hr |
| T = 2 | F = 82.45 | mm | Io = 42.94 | mm/hr |
| T = 2.5 | F = 109.90 | mm | Io = 57.24 | mm/hr |
| T = 3 | F = 130.68 | mm | Io = 68.06 | mm/hr |
| T = 3.5 | F = 147.45 | mm | Io = 76.80 | mm/hr |
| T = 4 | F = 161.54 | mm | Io = 84.14 | mm/hr |
| T = 4.5 | F = 173.70 | mm | Io = 90.47 | mm/hr |
| T = 5 | F = 184.39 | mm | Io = 96.04 | mm/hr |
| T = 10 | F = 251.88 | mm | Io = 131.19 | mm/hr |
| T = 20 | F = 316.62 | mm | Io = 164.91 | mm/hr |
| T = 50 | F = 400.42 | mm | Io = 208.55 | mm/hr |
| T = 100 | F = 463.22 | mm | Io = 241.26 | mm/hr |

Based on the above equations the rain fall intensity for various return periods is arrived.



| Minutes | | Critical | Rainfall Inter | sity (mm/hr) | |
|---------|--------|----------|----------------|--------------|----------|
| Minutes | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year |
| 5 | 79.30 | 177.30 | 242.20 | 385.00 | 445.40 |
| 10 | 73.60 | 164.60 | 224.90 | 357.50 | 413.60 |
| 15 | 68.70 | 153.70 | 209.90 | 333.70 | 386.00 |
| 20 | 64.40 | 144.10 | 196.80 | 312.80 | 361.90 |
| 25 | 60.60 | 135.60 | 185.20 | 294.40 | 340.60 |
| 30 | 57.30 | 128.00 | 174.90 | 278.10 | 321.70 |
| 35 | 54.20 | 121.30 | 165.70 | 263.40 | 304.70 |
| 40 | 51.50 | 115.20 | 157.40 | 250.30 | 289.50 |
| 45 | 49.10 | 109.80 | 149.90 | 238.30 | 275.70 |
| 50 | 46.80 | 104.80 | 143.10 | 227.50 | 263.20 |
| 55 | 44.80 | 100.20 | 136.90 | 217.60 | 251.70 |
| 60 | 42.9 | 96 | 131.2 | 208.6 | 241.3 |

Table 6: Critical Rainfall intensity be Least Square Method

The IDF curve for various return periods for a duration of 60 minutes has been given below:

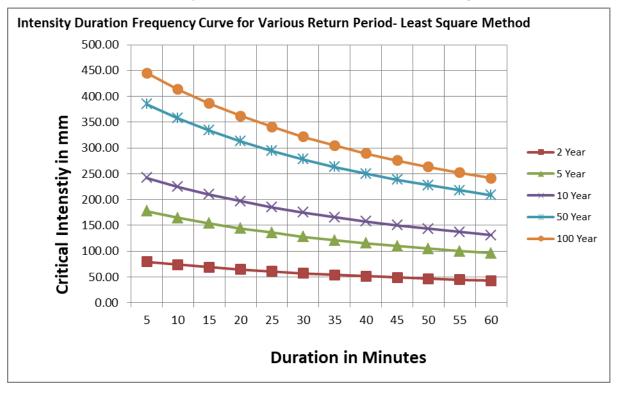


Figure 5: IDF Curve generation in Least Square Method





9.2. IMD 1/3rd Rule Method of Rainfall Intensity

Rainfall data being a random probability distribution, fit well with the theories of probability. Therefore, Gumbel's Extreme Value distribution can be ideally used to represent the rainfall Intensity Duration Frequency (IDF) relation.

The basic data required consists of rainfall details of the area under consideration for a substantial period. The rain fall details for 30 years period, obtained in respect of Agra region from the IMD has been used as the basic data.

IMD has suggested the 1/3rd rule for obtaining hourly rainfall from 24 hour data.

To generate shorter duration series (1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, hour series) the following IMD formula has been used.

 $P_t = P_{24} (t / 24)^{1/3}$

Where Pt = Rainfall of t hours duration in mm P24 = Daily Rainfall value in mm t = Shorter duration in hours (1, 2, 3...)

The above Equation is used to generate the extreme value series of duration 1 to 12 hours in steps of 1 hour. The resulting series are given below:

| Veer | | | Hours | | | Verr | | | Hours | | |
|------|------------------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| Year | 1 | 2 | 6 | 12 | 24 | Year | 1 | 2 | 6 | 12 | 24 |
| 1981 | 126.50 | 159.40 | 229.90 | 289.70 | 365.00 | 1998 | 18.70 | 23.60 | 34.00 | 42.90 | 54.00 |
| 1982 | 66.40 | 83.60 | 120.60 | 152.00 | 191.50 | 1999 | 20.80 | 26.20 | 37.80 | 47.60 | 60.00 |
| 1985 | 98.80 | 124.50 | 179.50 | 226.20 | 285.00 | 2000 | 9.40 | 11.80 | 17.00 | 21.40 | 27.00 |
| 1986 | 20.80 | 26.20 | 37.80 | 47.60 | 60.00 | 2001 | 5.60 | 7.00 | 10.10 | 12.80 | 16.10 |
| 1987 | 173.30 | 218.40 | 315.00 | 396.90 | 500.00 | 2002 | 23.00 | 28.90 | 41.70 | 52.50 | 66.20 |
| 1988 | 24.00 | 30.20 | 43.60 | 54.90 | 69.20 | 2003 | 19.10 | 24.00 | 34.60 | 43.70 | 55.00 |
| 1989 | 29.70 | 37.40 | 53.90 | 67.90 | 85.60 | 2004 | 11.10 | 14.00 | 20.20 | 25.40 | 32.00 |
| 1990 | 5.20 | 6.60 | 9.40 | 11.90 | 15.00 | 2005 | 23.60 | 29.70 | 42.80 | 54.00 | 68.00 |
| 1991 | 2.80 | 3.50 | 5.10 | 6.40 | 8.10 | 2006 | 15.30 | 19.20 | 27.70 | 34.90 | 44.00 |
| 1992 | 17.70 | 22.30 | 32.10 | 40.50 | 51.00 | 2007 | 18.00 | 22.70 | 32.80 | 41.30 | 52.00 |
| 1993 | 70.70 | 89.10 | 128.50 | 161.90 | 204.00 | 2008 | 24.30 | 30.60 | 44.10 | 55.60 | 70.00 |
| 1994 | 19.10 | 24.00 | 34.60 | 43.70 | 55.00 | 2009 | 4.40 | 5.50 | 7.90 | 10.00 | 12.60 |
| 1995 | 17.00 | 21.40 | 30.90 | 38.90 | 49.00 | 2010 | 22.20 | 28.00 | 40.30 | 50.80 | 64.00 |
| 1996 | 62.40 | 78.60 | 113.40 | 142.90 | 180.00 | 2011 | 20.10 | 25.30 | 36.50 | 46.00 | 58.00 |
| 1997 | 11.80 | 14.90 | 21.40 | 27.00 | 34.00 | 2012 | 55.50 | 69.90 | 100.80 | 127.00 | 160.00 |
| | Average | | | | | | 34.577 | 43.550 | 62.800 | 79.143 | 99.710 |
| | Average Per Hour | | | | | | 34.577 | 21.775 | 10.467 | 6.595 | 4.155 |

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The rainfall (P_T) corresponding to a specific return period (T) using **the Gumbel's extreme value distribution** is given by:

 $P_T = \sigma + K_T s$

Where ${}^{\scriptscriptstyle \mathsf{t}}\!\sigma'$ is the mean value of the original series and ${}^{\scriptscriptstyle \mathsf{t}}\!s'$ its standard deviation.

K_T, the frequency factor given by:

KT values are calculated for different return periods using Gumbel's distribution

| $K_{T} = -\frac{\sqrt{6}}{\pi}$ | 0.5772 + | $\ln\left[\ln\left(\frac{T}{T-T}\right)\right]$ |]]} | | | |
|---------------------------------|----------|---|-------|-------|-------|-------|
| T (years) | 2 | 5 | 10 | 20 | 50 | 100 |
| Kτ | -0.164 | 0.719 | 1.305 | 1.866 | 2.592 | 3.137 |

Based on the above equation rainfall intensities for various return periods are calculated and furnished below:

| Minutes | | | RETURN PER | IODS | |
|---------|--------|--------|------------|---------|----------|
| | 2 Year | 5 Year | 10 Year | 50 Year | 100 Year |
| 5 | 145.5 | 326.73 | 447.01 | 711.17 | 823.03 |
| 10 | 91.6 | 205.72 | 281.46 | 447.79 | 518.23 |
| 15 | 69.93 | 157.02 | 214.82 | 341.76 | 395.51 |
| 20 | 57.73 | 129.63 | 177.35 | 282.15 | 326.53 |
| 25 | 49.75 | 111.72 | 152.84 | 243.16 | 281.41 |
| 30 | 44.05 | 98.92 | 135.33 | 215.31 | 249.17 |
| 35 | 39.74 | 89.25 | 122.1 | 194.26 | 224.82 |
| 40 | 36.37 | 81.66 | 111.71 | 177.72 | 205.68 |
| 45 | 33.63 | 75.51 | 103.31 | 164.35 | 190.2 |
| 50 | 31.34 | 70.37 | 96.28 | 153.18 | 177.27 |
| 55 | 29.41 | 66.05 | 90.36 | 143.76 | 166.37 |
| 60 | 27.77 | 62.32 | 85.25 | 135.61 | 156.94 |

The IDF curve has been generated for various return periods.



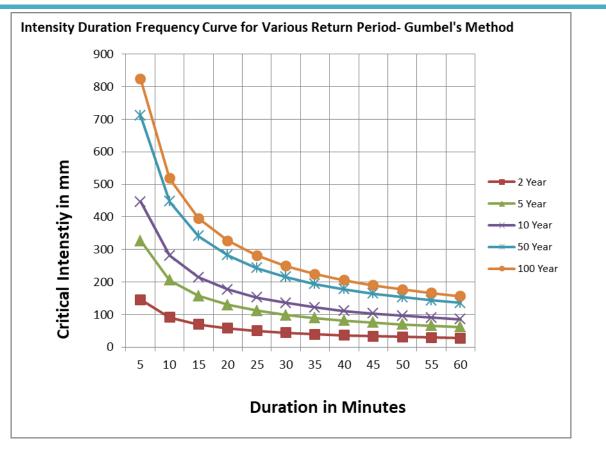


Figure 6: IDF Curve generation by Gumbel's Method

9.3. Comparison of values

The rainfall intensity for various return periods arrived by least square method and Gumbel's method are compared and the comparative table is given below.

| Intensity of rain fall in MM/HOUR | | | | | | | | |
|-----------------------------------|------------------------|-------|--------|--------|--------|--|--|--|
| Method | RETURN PERIOD IN YEARS | | | | | | | |
| | 2 | 5 | 10 | 50 | 100 | | | |
| Gumbel's Method | 28.20 | 62.55 | 85.34 | 135.41 | 156.61 | | | |
| Least Square Method | 42.90 | 96.00 | 131.20 | 208.60 | 241.30 | | | |

Table 9: Comparison of Rainfall Intensity

Based on the above values a chart is drawn and shown below:





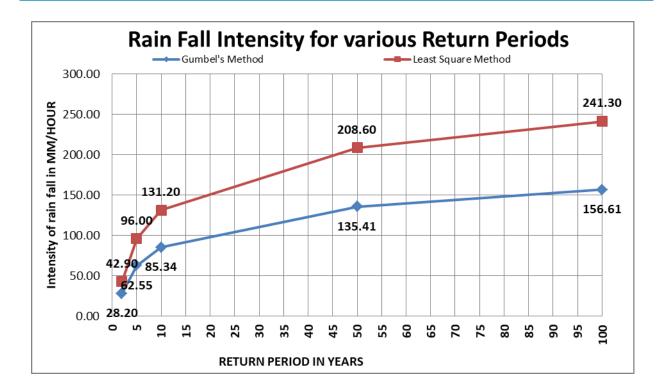


Figure 7: Graph showing the comparison of Rainfall Intensity by LSM and IMD 1/3rd Rule

9.4. Comparison of values

As already mentioned, it is seen that the rain fall data, obtained from IMD, has exceeded the average rain fall only for 9 years, and for major periods the annual rain fall are below average.

Therefore the values, as given below, arrived from Annual exceedance 1/3rd rule with Gumbel's method, suits to Agra region, are adopted for calculating the storm water flow and for designing the Storm water drainage system.

| Return Period in Years | Intensity of rain fall in mm / hr. |
|-------------------------------|------------------------------------|
| 2 | 28.20 |





10.0 Delineation of Strom Water Drainage Zones

The whole catchment area of Taj east drain has been divided into 7 storm water drainage catchment zones.

The total catchment area considered for this project is about 2369 Hect (or) 23.69.Sq.km.. The details of the catchments, drainage plus flow accumulation are shown in the figure 7.

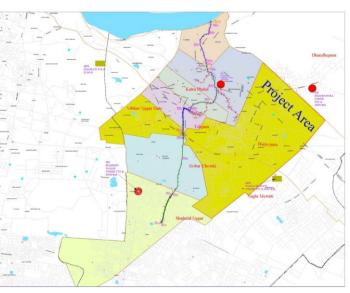


Figure 8: Details of catchment and flow details

The objective is to assess the problems and to identify with the aid of modern hydrological and hydraulic modelling techniques, measures to alleviate the problems along the drain. These catchments have different characteristic of their own have different types of land use pattern that affected the discharges. They have different soil characteristics; different permeability and flood absorption characteristic.

| Chainage Number | Label | Start Node | Stop Node | Length (Scaled) (m) | Flow (m³/s) | Capacity (Full Flow) (m ³ /s) | Flow / Capacity (Design) (%) | System CA (ha) |
|-----------------------|---------|---------------|--------------|---------------------------|----------------|---|---------------------------------------|-------------------|
| 0 to 60 | CO-1082 | CH-0 | CH-60 | 55.06 | 0.30 | 0.87 | 34.10 | 2.09 |
| | CO-1080 | CH-60 | CH-270 | 210.27 | 0.74 | 1.05 | 70.90 | 5.60 |
| 60 to 520 | CO-1077 | CH-270 | CH-390 | 122.47 | 0.75 | 2.55 | 29.50 | 6.60 |
| | CO-1074 | CH-390 | CH-520 | 130.38 | 0.86 | 1.42 | 60.50 | 7.77 |
| 520 to 520-1 (Cul) | CO-1096 | CH-520 | CH-520-1 | 8.92 | 0.93 | 16.27 | 5.70 | 8.86 |
| 810 to 930 | CO-1091 | CH-810 | CH-930 | 118.73 | 1.43 | 1.67 | 85.80 | 14.58 |
| 930 to 1140 | CO-1097 | CH-930 | CH-1140 | 211.8 | 1.57 | 1.24 | 126.60 | 16.28 |
| 1140 to 1500 | CO-1101 | CH-1140 | CH-1500 | 358.27 | 1.67 | 2.87 | 58.00 | 17.84 |
| 1500 to 1520 | CO-1183 | CH-1500 | CH-1520 | 25.57 | 1.69 | 6.29 | 26.90 | 18.65 |
| 1520 to 1532 | CO-1107 | CH-1520 | CH-1532 | 12.66 | 2.09 | 6.37 | 32.80 | 23.05 |
| 1532 to 1800 | CO-141 | CH-1532 | CH-1800 | 261.56 | 2.58 | 6.30 | 40.90 | 28.44 |
| | CO-147 | CH-1800 | CH-1940 | 144.1 | 2.66 | 4.03 | 66.10 | 29.74 |
| 1800 to 2040 | CO-151 | CH-1940 | CH-1950 | 9.36 | 2.72 | 4.03 | 67.50 | 30.66 |
| | CO-152 | CH-1950 | CH-2040 | 97.67 | 2.77 | 4.03 | 68.90 | 31.32 |
| | | | | | | | Total | 241.474 |

Table 11: Left Side Drain

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| Table 12: Right Side Drain |
|----------------------------|
|----------------------------|

| Chainage Number | Label | Start Node | Stop Node | Length (Scaled) (m) | Flow (m³/ s) | Capacity (Full Flow) (m ³ /s) | Flow / Capacity (Design) (%) | System CA (ha) |
|--------------------|---------|---------------|--------------|---------------------------|--------------------|---|---------------------------------------|----------------------|
| 0-1 to 60-1 | CO-1072 | CH-0-1 | CH-60-1 | 58.55 | 0.30 | 0.42 | 71.90 | 2.13 |
| 60-1 to 60 (Cul) | CO-1086 | CH-60-1 | CH-60 | 8.45 | 0.32 | 4.92 | 6.50 | 2.42 |
| 90-1 to 380-1 | CO-189 | CH-90-1 | CH-380-1 | 291.46 | 0.12 | 1.99 | 6.20 | 0.87 |
| 380-1 to 520-1 | CO-193 | CH-380-1 | CH-520-1 | 141.67 | 0.24 | 2.74 | 8.90 | 2.05 |
| 520-1 to 680 | CO-1071 | CH-520-1 | CH-680 | 160.10 | 1.23 | 1.31 | 93.40 | 11.70 |
| 680 to 810 | CO-1090 | CH-680 | CH-810 | 125.54 | 1.32 | 3.29 | 40.10 | 13.20 |
| 1440-1 to 1500-1 | CO-1196 | CH-1440-1 | CH-1500-1 | 59.69 | 0.02 | 1.47 | 1.3 | 0.1385 |
| 1500-1 to 1520-1 | CO-1185 | CH-1500-1 | CH-1520-1 | 22.2 | 0.02 | 5.66 | 0.4 | 0.1679 |
| 1520-1 to 1532-1 | CO-1108 | CH-1520-1 | CH-1532-1 | 12.00 | 0.85 | 2.10 | 40.40 | 9.36 |
| | CO-1110 | CH-1532-1 | CH-1800-1 | 265.05 | 2.18 | 2.98 | 73.30 | 24.23 |
| 1532-1 to 2010-1 | CO-1116 | CH-1800-1 | CH-1830-1 | 140.97 | 2.21 | 2.98 | 74.30 | 25.03 |
| | CO-1121 | CH-1830-1 | CH-2010-1 | 90.79 | 2.20 | 2.98 | 73.90 | 25.15 |
| 2010-1 to 2040 | CO-1120 | CH-2010-1 | CH-2040 | 7.79 | 2.25 | 2.98 | 75.60 | 25.91 |
| | | | | | | | Total | 142.36 |

Table 13: Single Drain

| Chainage Number | Label | Start Node | Stop Node | Length (Scaled) (m) | Flow (m³/s) | Capacity (Full Flow) (m ³ /s) | Flow / Capacity (Design) (%) | System CA (ha) |
|--------------------|---------|---------------|--------------|---------------------------|----------------|---|---------------------------------------|-------------------|
| 2040 to 2130 | CO-155 | CH-2040 | CH-2130 | 88.42 | 5.01 | 2.21 | 227.10 | 57.69 |
| 2130 to 2190 | CO-158 | CH-2130 | CH-2190 | 60.18 | 5.04 | 5.52 | 91.20 | 58.42 |
| 2190 to 2270 | CO-159 | CH-2190 | CH-2270 | 84.02 | 5.09 | 16.70 | 30.50 | 59.21 |
| 2270 to 2340 | CO-160 | CH-2270 | CH-2340 | 120.45 | 5.14 | 9.32 | 55.20 | 59.95 |
| 2340 to 2430 | CO-1146 | CH-2340 | CH-2430 | 35.68 | 5.24 | 26.46 | 19.80 | 61.45 |
| | CO-162 | CH-2430 | CH-2460 | 29.6 | 5.28 | 57.09 | 9.20 | 61.92 |
| 2430 to 2700 | CO-163 | CH-2460 | CH-2520 | 59.27 | 5.33 | 33.86 | 15.70 | 62.60 |
| 2.00 10 2700 | CO-164 | CH-2520 | CH-2580 | 59.93 | 5.38 | 11.52 | 46.70 | 63.37 |
| | CO-165 | CH-2580 | CH-2610 | 32.12 | 5.43 | 41.52 | 13.10 | 64.16 |





| Chainage Number | Label | Start Node | Stop Node | Length (Scaled) (m) | Flow (m³/s) | Capacity (Full Flow) (m ³ /s) | Flow / Capacity (Design) (%) | System CA (ha) |
|--------------------|---------|---------------|--------------|---------------------------|----------------|---|---------------------------------------|-------------------|
| | CO-166 | CH-2610 | CH-2670 | 58.32 | 5.45 | 32.71 | 16.70 | 64.48 |
| | CO-167 | CH-2670 | CH-2700 | 30.36 | 5.46 | 54.68 | 10.00 | 64.74 |
| | CO-1143 | CH-2700 | CH-2730 | 30.93 | 5.73 | 74.14 | 7.70 | 68.04 |
| 2700 to 2850 | CO-1144 | CH-2730 | CH-2790 | 58.4 | 5.76 | 52.42 | 11.00 | 68.47 |
| | CO-169 | CH-2790 | CH-2850 | 60.88 | 5.77 | 55.64 | 10.40 | 68.69 |
| | CO-170 | CH-2850 | CH-2910 | 60.07 | 5.81 | 68.26 | 8.50 | 69.30 |
| 2850 to 2970 | CO-171 | CH-2910 | CH-2940 | 29.43 | 5.84 | 78.17 | 7.50 | 69.81 |
| | CO-172 | CH-2940 | CH-2970 | 28.64 | 5.91 | 73.36 | 8.10 | 70.79 |
| 2970 to 3030 | CO-173 | CH-2970 | CH-3000 | 29.34 | 6.04 | 92.90 | 6.50 | 72.35 |
| | CO-174 | CH-3000 | CH-3030 | 38.46 | 6.08 | 220.94 | 2.80 | 73.05 |
| 3030 to 3120 | CO-175 | CH-3030 | CH-3120 | 76.97 | 6.30 | 67.81 | 9.30 | 75.67 |
| 3120 to 3215 | CO-176 | CH-3120 | CB-3215 | 95.69 | 6.41 | 179.55 | 3.60 | 77.35 |
| 3215 to 3225 | CO-177 | CB-3215 | CH-3225 | 11.07 | 6.44 | 17.49 | 36.80 | 78.01 |
| | CO-178 | CH-3225 | CH-3300 | 74.53 | 6.47 | 9.28 | 69.70 | 78.59 |
| | CO-1193 | CH-3300 | CH-3390 | 90.09 | 6.48 | 10.38 | 62.40 | 79.25 |
| | CO-180 | CH-3390 | CH-3540 | 150.27 | 6.46 | 10.38 | 62.30 | 79.96 |
| | CO-1191 | CH-3540 | CH-3600 | 58.8 | 6.40 | 10.38 | 61.70 | 80.51 |
| | CO-1177 | CH-3600 | CH-3630 | 29.72 | 6.41 | 10.38 | 61.80 | 81.12 |
| 3225 to 4000 | CO-182 | CH-3630 | CH-3750 | 120.03 | 6.46 | 10.38 | 62.20 | 81.91 |
| | CO-183 | CH-3750 | CH-3810 | 59.92 | 6.43 | 10.38 | 61.90 | 82.59 |
| | CO-184 | CH-3810 | CH-3870 | 61.01 | 6.43 | 10.38 | 61.90 | 83.14 |
| | CO-185 | CH-3870 | CH-3900 | 30.1 | 6.42 | 10.38 | 61.80 | 83.54 |
| | CO-186 | CH-3900 | CH-3990 | 90.07 | 6.43 | 10.38 | 61.90 | 83.99 |
| | CO-187 | CH-3990 | OF-3 | 15.17 | 6.41 | 10.38 | 61.80 | 84.59 |
| | | | | | | | Total | 2,368.68 |

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11.0 Hydraulic Analysis of Taj East drain

The Runoff flow from these catchment drains into Taj east drains during rainy season only, the drains may flooded / overtopped during rainy season, this may be due to

- > The change in the land use,
- > Change in the rainfall pattern
- Reduction in the carrying capacity of drains due to dumping of solid wastes, vegetation growths, silting up of the beds and

The existing Land use detail has been used to arrive at the probable run off co-efficient for the calculations of discharges in the Macro drains. The cross sectional and longitudinal sectional details of drain have been carried out

For the analysis and adequacy check of the Taj east drain Bentley's StormCAD software has been used and the results are furnished in Annexure- II

12.0 Flood occurrence under various scenarios

The adequacy of the proposed sections, in respect of Taj east drain have been checked for the storm return periods of 2 year, and analysed. As per the analysis, the flooding will occur at the reaches that are indicated in RED colour, in the figures furnished below:

| Series Pa | nel Axes General Titles Walts | Paging Legend |
|------------|-------------------------------|---------------|
| | Gissel | |
| - 20 | Structure | Add |
| 1 R | HGL (Area) | Delete |
| d 2 | Pipe (Area) | |
| Ke R- | - EGL | Title |
| 1 Z- | - HGL | Close |
| | Annotation | |
| 100 | Annotation Table Labels | Change. |
| 检区 | Annotation Table | |

Figure 9:Legend



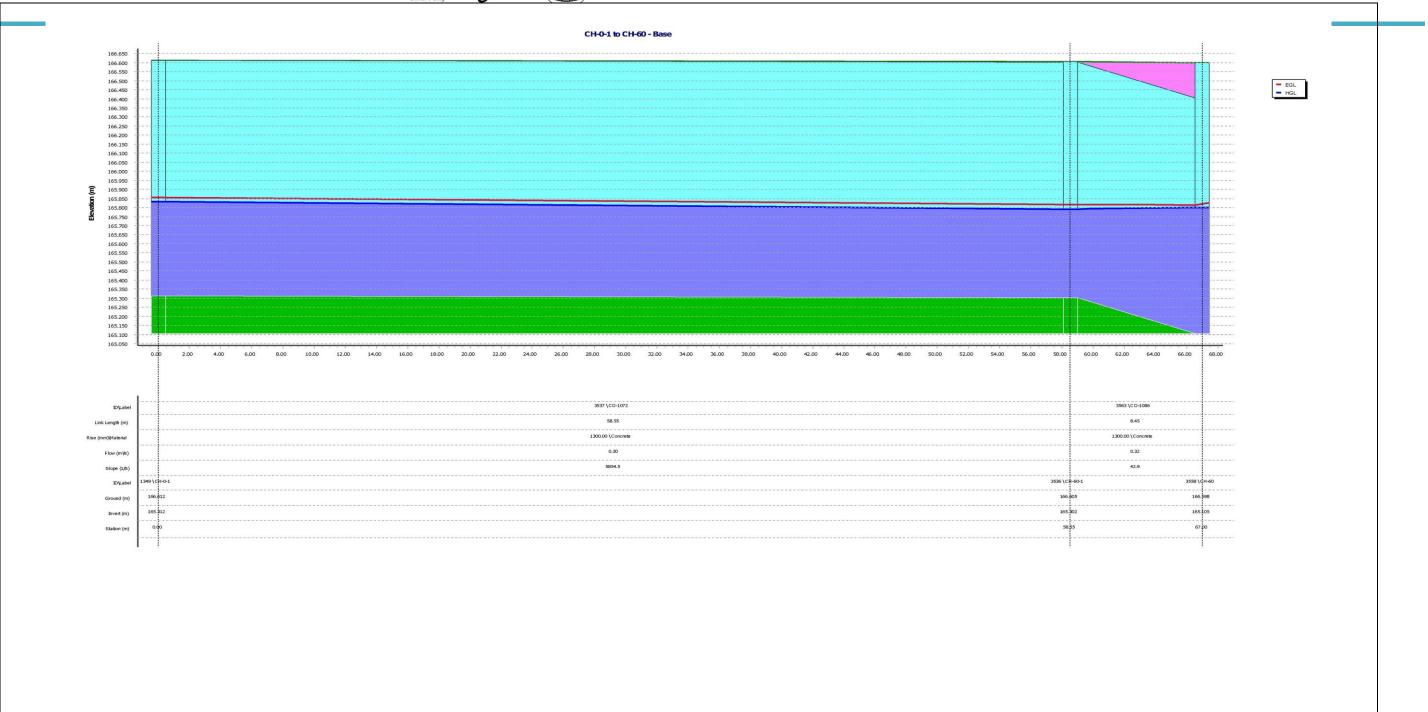
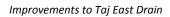


Figure 10: Flood occurring reaches for 2 years return period

36







Rise (mm)\Ma

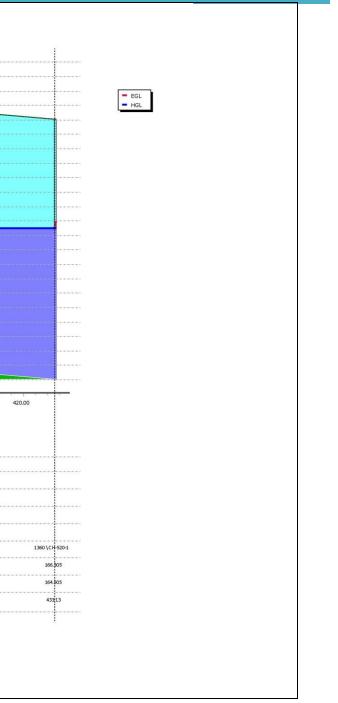
| Link Length (m) | | 291.46 | 141.67 |
|------------------|--------|-------------------|-------------------|
| se (mm)\Material | | 1300.00 \Concrete | 1800.00 \Concrete |
| Flow (m3/s) | | 0.12 | 0.24 |
| Slope (1/5) | | 578.3 | 708.3 |
| ID\Label | 50 \CH | 90-1 1358 / CH | 380-1 |
| Ground (m) | 166.66 | 0 156.3 | 05 |
| Invert (m) | 165.20 | 9 164.7 | 05 |
| Station (m) | 0.00 | 291 | 6 |
| | | | |
| | | | |

360.00

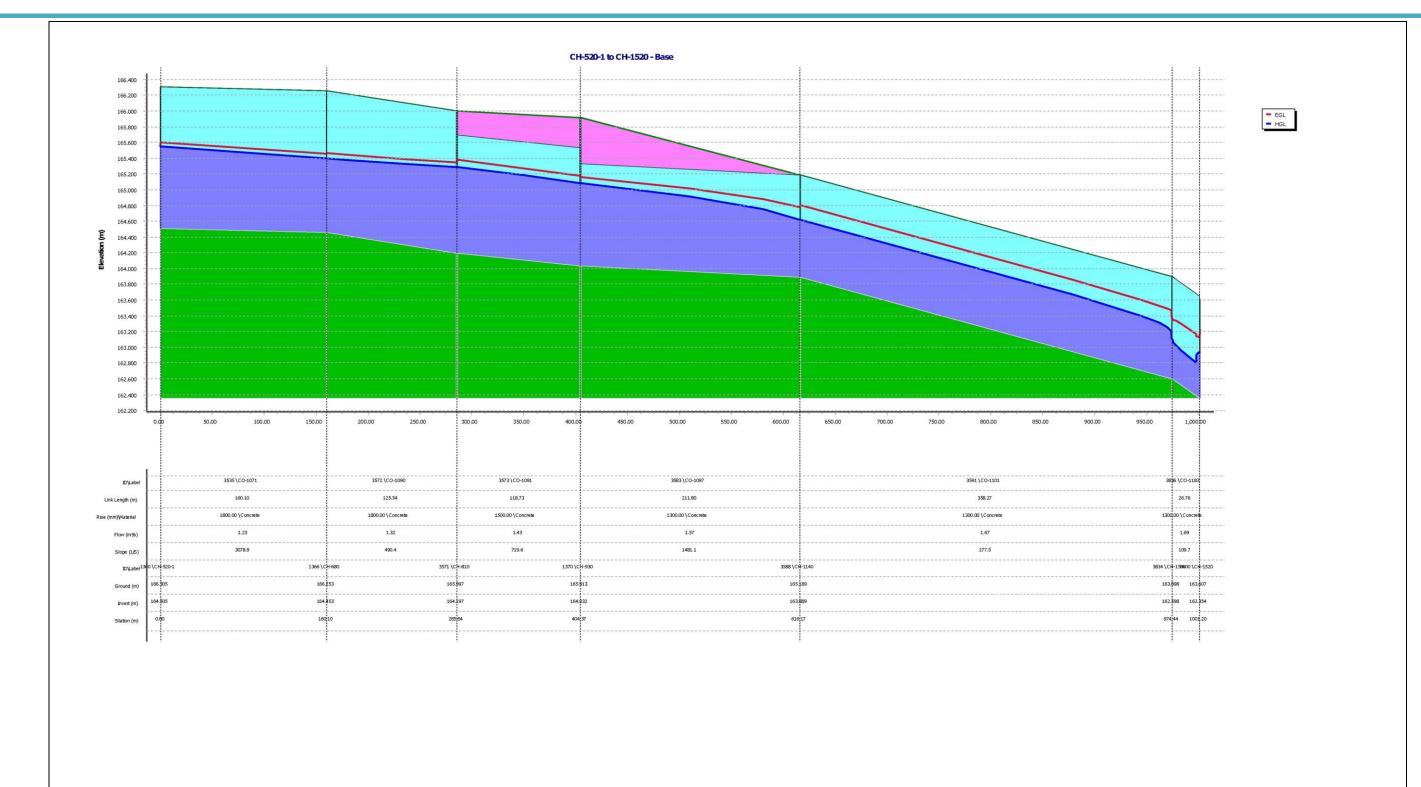
1361 \CO-193

380.00

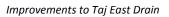
400.00



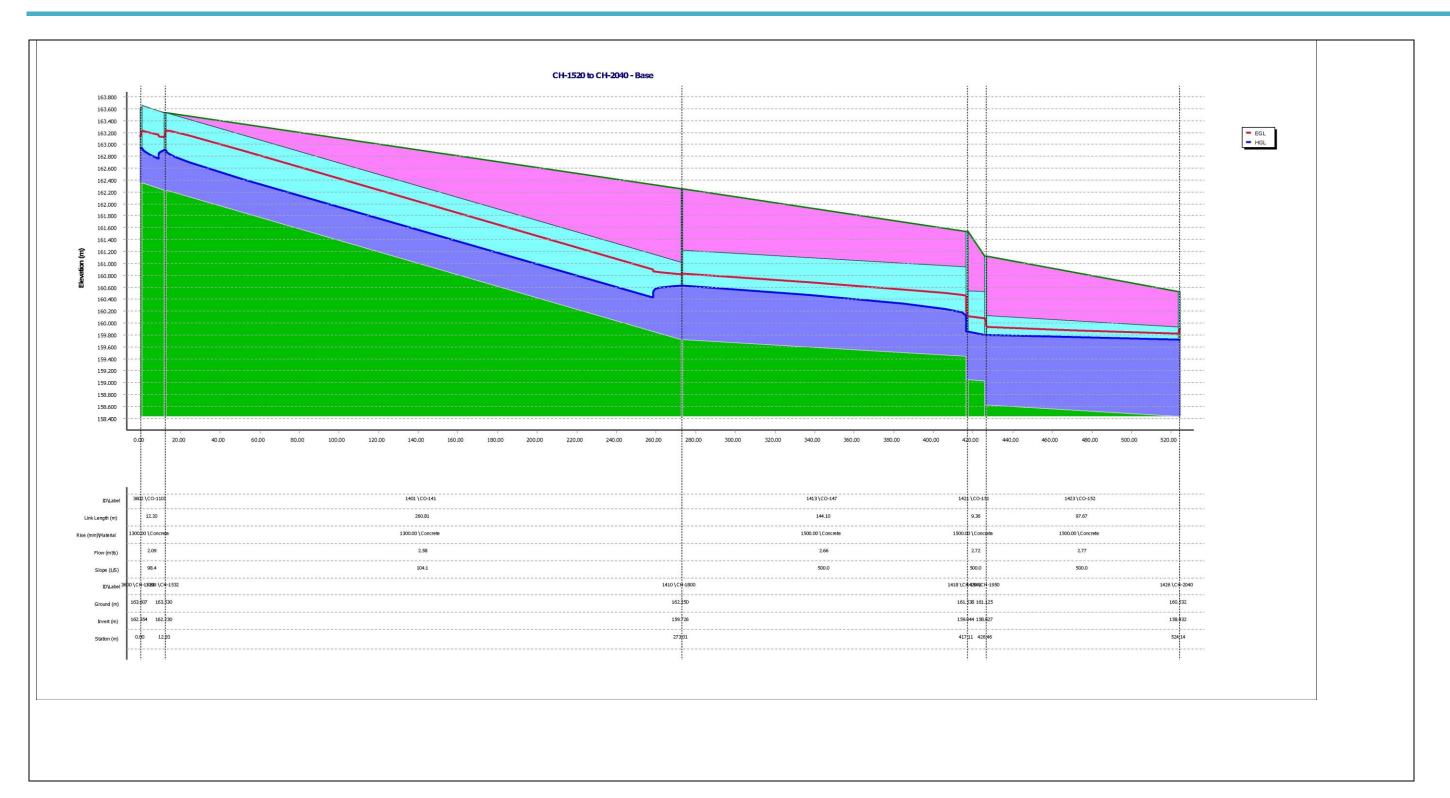




38

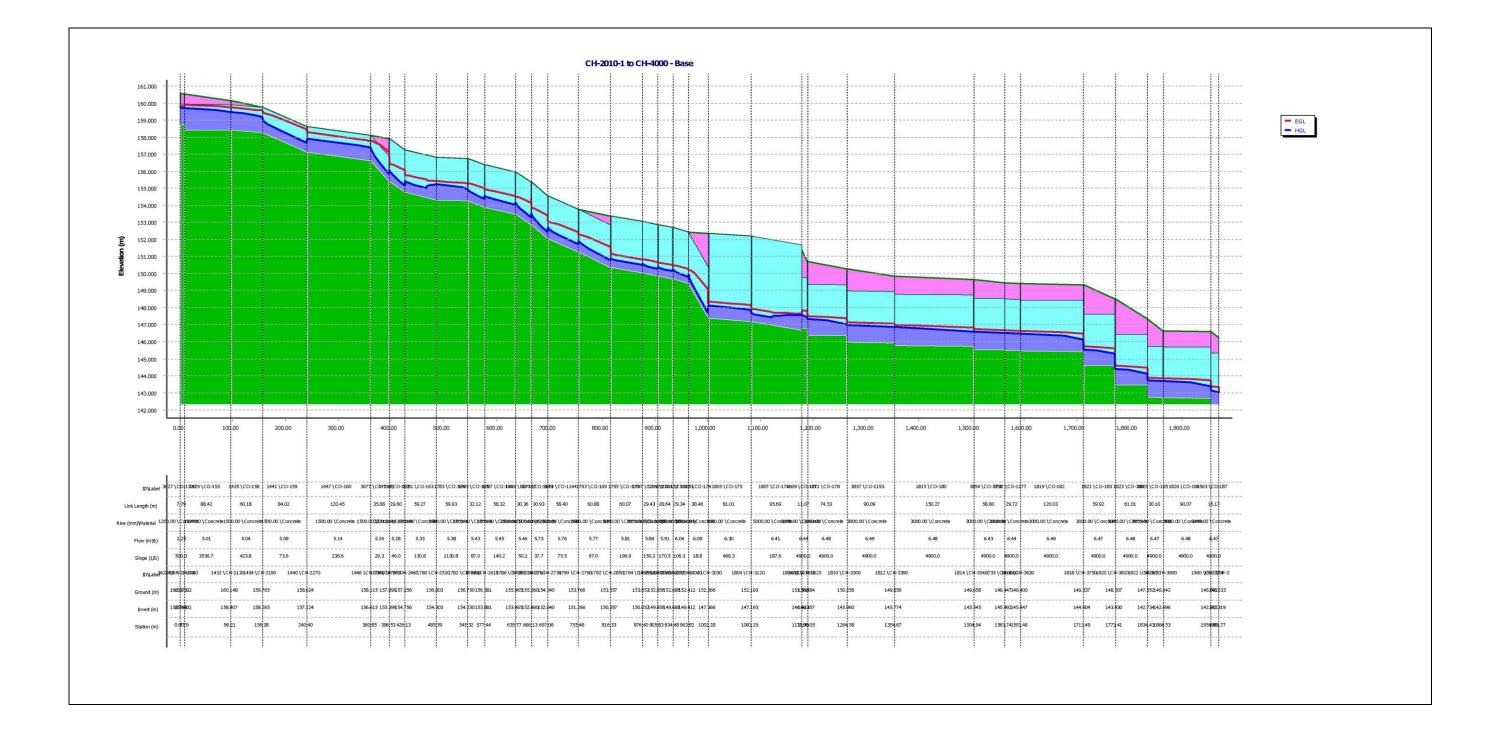






39

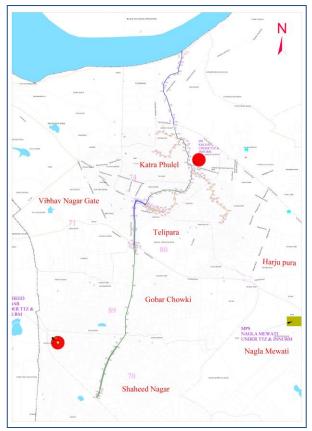






13.0 Improvements of Taj east drain

This drain originate from Shamshabad road and traverse through and terminates at river Yamuna. Length of Taj east drain is 4000 m and width of the channel varies from 0.90 m to 6 m. The following settlements fall in the Taj east drain catchment area Rajpur, Shamshabad Road, Vashistpuram, KalindiVihar Road, Bank Colony, Bagh Rajpur, Pakki Sarai, Lacchipura, Shaheed nagar, Kareem Nagar, GobarChauki, M.P. Pura, Harjupura, Gummat, PuraniMandi, sanjay colony, Taj Ganj, Navada, Patiram ki Bagichi, Sheik Bulakhi, Paak Tola, Basai Kalan, Marutam Nagar, Billochpura, Tajganj, Telipada, Kohai and Taj East Gate Road (Source: City Sanitation Plan, Agra, 2011).



The adequacy of drain section for various scenarios 2 years return periods have been analysed and the section of channel for 2 years return period has been modified and tabulated below:



Table 14: Left Side Drain

| Chainage Number | Label | Start Node | Stop Node | Elevation Ground (Start) (m) | Elevation Ground (Stop) (m) | Invert (Start) (m) | Invert (Stop) (m) | Length (Scaled) (m) | Conduit Description | Slope (Calculated) (1/S) | Velocity (m/s) | Flow (m³/s) | Capacity (Full Flow) (m³/s) | Flow / Capacity (Design) (%) |
|--------------------|---------|---------------|--------------|------------------------------------|-----------------------------------|--------------------------|-------------------------|---------------------------|------------------------|--------------------------------|-------------------|----------------|--------------------------------|---------------------------------|
| 0 to 60 | CO-1082 | CH-0 | CH-60 | 166.612 | 166.598 | 166.012 | 165.105 | 55.06 | SS-0.60 x 0.60 | 60.70 | 2.18 | 0.30 | 0.87 | 34.10 |
| | CO-1080 | CH-60 | CH-270 | 166.598 | 166.567 | 165.105 | 165.067 | 210.27 | SS-1.50 x 1.50 | 5533.40 | 0.51 | 0.74 | 1.05 | 70.90 |
| 60 to 520 | CO-1077 | CH-270 | CH-390 | 166.567 | 166.436 | 165.067 | 164.936 | 122.47 | SS-1.50 x 1.50 | 934.90 | 0.98 | 0.75 | 2.55 | 29.50 |
| | CO-1074 | CH-390 | CH-520 | 166.436 | 166.393 | 164.936 | 164.893 | 130.38 | SS-1.50 x 1.50 | 3032.20 | 0.66 | 0.86 | 1.42 | 60.50 |
| 520 to 520-1 (Cul) | CO-1096 | CH-520 | CH-520-1 | 166.393 | 166.305 | 164.893 | 164.505 | 8.92 | SS-1.50 x 1.50 | 23.00 | 3.58 | 0.93 | 16.27 | 5.70 |
| 810 to 930 | CO-1091 | CH-810 | CH-930 | 165.997 | 165.913 | 164.197 | 164.032 | 118.73 | SS-1.00 x 1.50 | 719.60 | 1.23 | 1.43 | 1.67 | 85.80 |
| 930 to 1140 | CO-1097 | CH-930 | CH-1140 | 165.913 | 165.189 | 164.032 | 163.889 | 211.8 | SS-1.20 x 1.30 | 1481.10 | 1.01 | 1.57 | 1.24 | 126.60 |
| 1140 to 1500 | CO-1101 | CH-1140 | CH-1500 | 165.189 | 163.898 | 163.889 | 162.598 | 358.27 | SS-1.20 x 1.30 | 277.50 | 1.91 | 1.67 | 2.87 | 58.00 |
| 1500 to 1520 | CO-1183 | CH-1500 | CH-1520 | 163.898 | 163.607 | 162.598 | 162.354 | 25.57 | SS-1.50 x 1.30 | 104.80 | 2.71 | 1.69 | 6.29 | 26.90 |
| 1520 to 1532 | CO-1107 | CH-1520 | CH-1532 | 163.607 | 163.53 | 162.354 | 162.23 | 12.66 | SS-1.50 x 1.30 | 102.10 | 2.91 | 2.09 | 6.37 | 32.80 |
| 1532 to 1800 | CO-141 | CH-1532 | CH-1800 | 163.53 | 162.25 | 162.23 | 159.726 | 261.56 | SS-1.50 x 1.30 | 104.40 | 3.06 | 2.58 | 6.30 | 40.90 |
| | CO-147 | CH-1800 | CH-1940 | 162.25 | 161.538 | 159.726 | 159.438 | 144.1 | SS-1.50 x 1.50 | 500.00 | 1.91 | 2.66 | 4.03 | 66.10 |
| 1800 to 2040 | CO-151 | CH-1940 | CH-1950 | 161.538 | 161.125 | 159.044 | 159.025 | 9.36 | SS-1.50 x 1.50 | 500.00 | 1.92 | 2.72 | 4.03 | 67.50 |
| | CO-152 | CH-1950 | CH-2040 | 161.125 | 160.532 | 158.627 | 158.432 | 97.67 | SS-1.80 x 1.50 | 500.00 | 1.93 | 2.77 | 4.03 | 68.90 |



Table 15: Right Side Drain

| Chainage Number | Label | Start Node | Stop Node | Elevation Ground (Start) (m) | Elevation Ground (Stop) (m) | Invert (Start) (m) | Invert (Stop) (m) | Length (Scaled) (m) | Conduit Description | Slope (Calculated) (1/S) | Velocity (m/s) | Flow (m³/s) | Capacity (Full Flow) (m³/s) | Flow / Capacity (Design) (%) |
|--------------------|---------|---------------|--------------|------------------------------------|-----------------------------------|--------------------------|-------------------------|---------------------------|------------------------|--------------------------------|-------------------|----------------|-----------------------------------|------------------------------------|
| 0-1 to 60-1 | CO-1072 | CH-0-1 | CH-60-1 | 166.612 | 166.605 | 165.312 | 165.302 | 58.55 | SS-0.90 x 1.30 | 5,854.50 | 0.39 | 0.30 | 0.42 | 71.90 |
| 60-1 to 60 (Cul) | CO-1086 | CH-60-1 | CH-60 | 166.605 | 166.598 | 165.302 | 165.105 | 8.45 | SS-0.90 x 1.30 | 42.90 | 2.37 | 0.32 | 4.92 | 6.50 |
| 90-1 to 380-1 | CO-189 | CH-90-1 | CH-380-1 | 166.660 | 166.505 | 165.209 | 164.705 | 291.46 | SS-1.20 x 1.30 | 578.30 | 0.68 | 0.12 | 1.99 | 6.20 |
| 380-1 to 520-1 | CO-193 | CH-380-1 | CH-520-1 | 166.505 | 166.305 | 164.705 | 164.505 | 141.67 | SS-1.20 x 1.80 | 708.30 | 0.80 | 0.24 | 2.74 | 8.90 |
| 520-1 to 680 | CO-1071 | CH-520-1 | CH-680 | 166.305 | 166.253 | 164.505 | 164.453 | 160.10 | SS-1.20 x 1.80 | 3,078.90 | 0.68 | 1.23 | 1.31 | 93.40 |
| 680 to 810 | CO-1090 | CH-680 | CH-810 | 166.253 | 165.997 | 164.453 | 164.197 | 125.54 | SS-1.20 x 1.80 | 490.40 | 1.45 | 1.32 | 3.29 | 40.10 |
| 1440-1 to 1500-1 | CO-1196 | CH-1440-1 | CH-1500-1 | 164.723 | 163.782 | 164.223 | 162.582 | 59.69 | SS-0.90 x 0.50 | 36.4 | 0.9 | 0.02 | 1.47 | 1.3 |
| 1500-1 to 1520-1 | CO-1185 | CH-1500-1 | CH-1520-1 | 163.782 | 163.607 | 162.582 | 161.742 | 22.2 | SS-0.90 x 1.20 | 26.4 | 1.06 | 0.02 | 5.66 | 0.4 |
| 1520-1 to 1532-1 | CO-1108 | CH-1520-1 | CH-1532-1 | 163.607 | 163.530 | 161.742 | 161.730 | 12.00 | SS-1.50 x 1.20 | 1,000.00 | 1.10 | 0.85 | 2.10 | 40.40 |
| | CO-1110 | CH-1532-1 | CH-1800-1 | 163.530 | 162.227 | 160.957 | 160.427 | 265.05 | SS-1.50 x 1.20 | 500.00 | 1.83 | 2.18 | 2.98 | 73.30 |
| 1532-1 to 2010-1 | CO-1116 | CH-1800-1 | CH-1830-1 | 162.227 | 161.303 | 159.785 | 159.503 | 140.97 | SS-1.50 x 1.20 | 500.00 | 1.83 | 2.21 | 2.98 | 74.30 |
| | CO-1121 | CH-1830-1 | CH-2010-1 | 161.303 | 160.573 | 158.954 | 158.773 | 90.79 | SS-1.50 x 1.20 | 500.00 | 1.83 | 2.20 | 2.98 | 73.90 |
| 2010-1 to 2040 | CO-1120 | CH-2010-1 | CH-2040 | 160.573 | 160.532 | 158.748 | 158.732 | 7.79 | SS-1.80 x 1.20 | 500.00 | 1.84 | 2.25 | 2.98 | 75.60 |



Table 16: Single Drain

| Chainage Number | Label | Start Node | Stop Node | Elevation Ground (Start) (m) | Ground (St | vert Invert art) (Stop) m) (m) | Length (Scaled) (m) | Conduit Description | Slope (Calculated) (1/S) | Velocity (m/s) | Flo (m ³ | ow ^s /s) | Capacity (Full Flow) (m ³ /s) | Flow / Capacity (Design) (%) |
|--------------------|---------|------------|-----------|------------------------------------|------------|--------------------------------------|---------------------------|------------------------|--------------------------------|-------------------|------------------------|------------------------|--|---------------------------------------|
| 2040 to 2130 | CO-155 | CH-2040 | CH-2130 | 160.532 | 160.148 | 158.432 | 158.407 | 88.42 | SS-2.00 x 1.50 | 3,536.70 | 1.67 | 5.01 | 2.21 | 227.10 |
| 2130 to 2190 | CO-158 | CH-2130 | CH-2190 | 160.148 | 159.765 | 158.407 | 158.265 | 60.18 | SS-2.00 x 1.50 | 423.80 | 2.15 | 5.04 | 5.52 | 91.20 |
| 2190 to 2270 | CO-159 | CH-2190 | CH-2270 | 159.765 | 158.624 | 158.265 | 157.124 | 84.02 | SS-2.40 x 1.50 | 73.60 | 3.99 | 5.09 | 16.70 | 30.50 |
| 2270 to 2340 | CO-160 | CH-2270 | CH-2340 | 158.624 | 158.115 | 157.124 | 156.615 | 120.45 | SS-2.40 x 1.50 | 236.60 | 2.66 | 5.14 | 9.32 | 55.20 |
| 2340 to 2430 | CO-1146 | CH-2340 | CH-2430 | 158.115 | 157.899 | 156.615 | 155.399 | 35.68 | SS-2.40 x 1.50 | 29.30 | 5.50 | 5.24 | 26.46 | 19.80 |
| | CO-162 | CH-2430 | CH-2460 | 157.899 | 157.256 | 155.399 | 154.756 | 29.6 | SS-3.00 x 2.50 | 46.00 | 4.50 | 5.28 | 57.09 | 9.20 |
| | CO-163 | CH-2460 | CH-2520 | 157.256 | 156.803 | 154.756 | 154.303 | 59.27 | SS-3.00 x 2.50 | 130.80 | 3.19 | 5.33 | 33.86 | 15.70 |
| 2420 to 2700 | CO-164 | CH-2520 | CH-2580 | 156.803 | 156.75 | 154.303 | 154.25 | 59.93 | SS-3.00 x 2.50 | 1,130.80 | 1.51 | 5.38 | 11.52 | 46.70 |
| 2430 to 2700 | CO-165 | CH-2580 | CH-2610 | 156.75 | 156.381 | 154.25 | 153.881 | 32.12 | SS-3.00 x 2.50 | 87.00 | 3.68 | 5.43 | 41.52 | 13.10 |
| | CO-166 | CH-2610 | CH-2670 | 156.381 | 155.965 | 153.881 | 153.465 | 58.32 | SS-3.00 x 2.50 | 140.20 | 3.14 | 5.45 | 32.71 | 16.70 |
| | CO-167 | CH-2670 | CH-2700 | 155.965 | 155.36 | 153.465 | 152.86 | 30.36 | SS-3.00 x 2.50 | 50.20 | 4.43 | 5.46 | 54.68 | 10.00 |
| | CO-1143 | CH-2700 | CH-2730 | 155.36 | 154.54 | 152.86 | 152.04 | 30.93 | SS-3.40 x 2.50 | 37.70 | 4.78 | 5.73 | 74.14 | 7.70 |
| 2700 to 2850 | CO-1144 | CH-2730 | CH-2790 | 154.54 | 153.766 | 152.04 | 151.266 | 58.4 | SS-3.40 x 2.50 | 75.50 | 3.82 | 5.76 | 52.42 | 11.00 |
| | CO-169 | CH-2790 | CH-2850 | 153.766 | 153.357 | 151.266 | 150.357 | 60.88 | SS-3.40 x 2.50 | 67.00 | 3.98 | 5.77 | 55.64 | 10.40 |
| | CO-170 | CH-2850 | CH-2910 | 153.357 | 153.052 | 150.357 | 150.052 | 60.07 | SS-5.00 x 3.00 | 196.90 | 2.53 | 5.81 | 68.26 | 8.50 |
| 2850 to 2970 | CO-171 | CH-2910 | CH-2940 | 153.052 | 152.856 | 150.052 | 149.856 | 29.43 | SS-5.00 x 3.00 | 150.20 | 2.76 | 5.84 | 78.17 | 7.50 |
| | CO-172 | CH-2940 | CH-2970 | 152.856 | 152.688 | 149.856 | 149.688 | 28.64 | SS-5.00 x 3.00 | 170.50 | 2.66 | 5.91 | 73.36 | 8.10 |
| 2070 to 2020 | CO-173 | CH-2970 | CH-3000 | 152.688 | 152.412 | 149.688 | 149.412 | 29.34 | SS-5.00 x 3.00 | 106.30 | 2.70 | 6.04 | 92.90 | 6.50 |
| 2970 to 3030 | CO-174 | CH-3000 | CH-3030 | 152.412 | 152.366 | 149.412 | 147.366 | 38.46 | SS-5.00 x 3.00 | 18.80 | 6.50 | 6.08 | 220.94 | 2.80 |
| 3030 to 3120 | CO-175 | CH-3030 | CH-3120 | 152.366 | 152.193 | 147.366 | 147.193 | 76.97 | SS-4.00 x 5.00 | 444.90 | 2.11 | 6.30 | 67.81 | 9.30 |
| 3120 to 3215 | CO-176 | CH-3120 | CB-3215 | 152.193 | 151.36 | 147.193 | 146.683 | 95.69 | SS-6.00 x 5.00 | 187.60 | 2.53 | 6.41 | 179.55 | 3.60 |

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| Chainage Number | Label | Start Node | Stop Node | Elevation Ground (Start) (m) | Elevation Ground (Stop) (m) | Invert (Start) (m) | Invert (Stop) (m) | Length (Scaled) (m) | Conduit Description | Slope (Calculated) (1/S) | Velocity (m/s) | Flow (m³/s) | Capacity (Full Flow) (m³/s) | Flow / Capacity (Design) (%) |
|--------------------|---------|---------------|--------------|------------------------------------|-----------------------------------|-----------------------|----------------------|---------------------------|------------------------|--------------------------------|-------------------|----------------|-----------------------------------|---------------------------------------|
| | | | | | | | | | | | | | | |
| 3215 to 3225 | CO-177 | CB-3215 | CH-3225 | 151.36 | 150.684 | 146.776 | 146.77 | 11.07 | SS-6.00 x 5.00 | 1,727.00 | 0.91 | 6.44 | 17.49 | 36.80 |
| 3225 to 4000 | CO-178 | CH-3225 | CH-3300 | 150.684 | 150.256 | 146.354 | 146.342 | 74.53 | SS-6.00 x 5.00 | 6,137.40 | 0.91 | 6.47 | 9.28 | 69.70 |
| | CO-1193 | CH-3300 | CH-3390 | 150.256 | 149.856 | 145.96 | 145.942 | 90.09 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.48 | 10.38 | 62.40 |
| | CO-180 | CH-3390 | CH-3540 | 149.856 | 149.658 | 145.774 | 145.744 | 150.27 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.46 | 10.38 | 62.30 |
| | CO-1191 | CH-3540 | CH-3600 | 149.658 | 149.447 | 145.545 | 145.533 | 58.8 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.40 | 10.38 | 61.70 |
| | CO-1177 | CH-3600 | CH-3630 | 149.447 | 149.4 | 145.492 | 145.486 | 29.72 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.41 | 10.38 | 61.80 |
| | CO-182 | CH-3630 | CH-3750 | 149.4 | 149.337 | 145.447 | 145.423 | 120.03 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.46 | 10.38 | 62.20 |
| | CO-183 | CH-3750 | CH-3810 | 149.337 | 148.507 | 144.604 | 144.592 | 59.92 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.43 | 10.38 | 61.90 |
| | CO-184 | CH-3810 | CH-3870 | 148.507 | 147.352 | 143.45 | 143.438 | 61.01 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.43 | 10.38 | 61.90 |
| | CO-185 | CH-3870 | CH-3900 | 147.352 | 146.642 | 142.734 | 142.728 | 30.1 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.42 | 10.38 | 61.80 |
| | CO-186 | CH-3900 | CH-3990 | 146.642 | 146.592 | 142.696 | 142.678 | 90.07 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.43 | 10.38 | 61.90 |
| | | CH-3990 | OF-3 | 146.592 | 146.233 | 142.322 | 142.319 | 15.17 | SS-6.00 x 5.00 | 4,900.00 | 0.91 | 6.41 | 10.38 | 61.80 |

Replacement / Proposed drains

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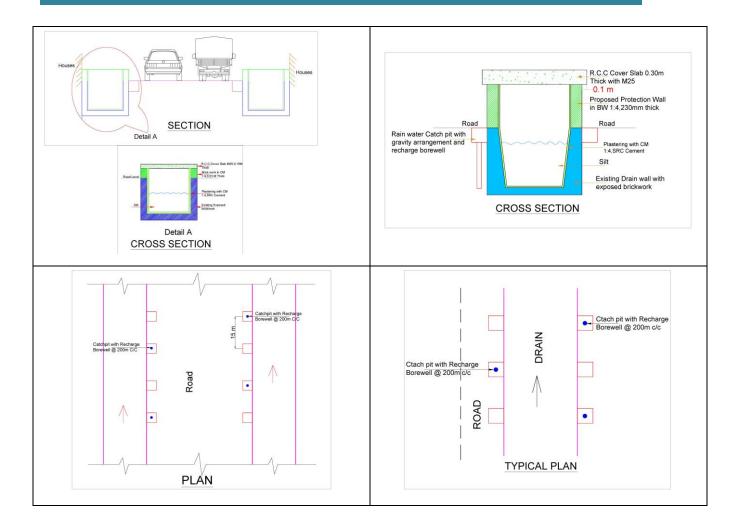


14.0 Proposals

- From chainage from 0m to 680m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain
 - 1. Rising of side wall
 - 2. Plastering of exposed brickwork inside of drain
 - 3. Providing RCC cover slab
 - 4. Providing grating arrangements with rain water harvesting structures
- From chainage from 680m to 810m the existing drain size is closed with RCC slab and serving as road. So, no improvement works are proposed except desilting and disposing of silt and solid waste.
- From chainage from 810m to 1800 (R), 1520 (L) the existing drain size is inadequate for hydraulic adequacy. The following works are proposed for strengthening of drain
 - 1. Construction of new RCC drain with cover slab and grating arrangement with rain water harvesting structures
- From chainage from 2040m to 3120m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain
 - 1. Rising of protection wall on both side of the drain with brickwork
 - 2. Plastering of inside exposed brickwork
 - 3. Providing cover slab with ventilation shaft for air ventilation
 - 4. Providing grating arrangements with rain water harvesting structures
- From chainage from 3120m to 3215m the existing drain size is adequate for hydraulic adequacy. The following works are proposed for strengthening of drain
 - 5. Construction of new side wall
 - 6. Plastering of inside exposed brickwork
 - 7. Providing cover slab with ventilation shaft for air ventilation
 - 8. Providing grating arrangements with rain water harvesting structures
- From chainage from 3215m to 4000m new adequate drain size is proposed for hydraulic adequacy. The following works are proposed for construction of new drain
 - 1. Construction of new RCC drain as per the hydraulic and structural design requirements with rain water harvesting structures
- Apart from the above proposal wherever lateral drains join the main drain screen chamber is proposed to avoid mixing of solid waste into main drain













15.0 Way forward

Improving the structural stability of the drain by refurbishment of civil structures, as per the physical condition assessment carried out. Rehabilitation works such as construction of drain side retaining wall, raising of drain side wall above ground level to prevent dumping of solid waste and enable safety of adjoining residents. Wherever drain wall doesn't exist new RCC drain side walls are proposed

The sewerage improvement plan for ABD area is under progress. By implementing the smart city project the 100% coverage of sewerage facilities for Taj east drain will be covered. House sewer connections for newly laid pipes and gap in sewer connections shall be ensured to combat sewage inflow into Taj east drain. Over the period of time after completing Smart City Project zero discharge of sewage into Taj east drain shall be ensured

The comprehensive solid waste management is also part of Smart City project and by implementation of this project effective door to door solid waste collection will be implemented. Hence dumping of solid waste into drain will be nullified

So, over a period of time after completion of Smart city mission project the Taj east drain will be free from pollutants from domestic sewage and solid waste and only carry storm water discharge into river Yamuna.







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